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## **Amendments to the Specification:**

Page 20, lines 2-9, please replace the paragraph with the following amended paragraph:

It should be noted that the light homogenizing optical sheet exhibits fold symmetry across a plane at its center of thickness. In such a case, a reflective light homogenizing sheet 210 can be formed as in Fig. 17A such that the first microlens surface 20(21) is utilized for both the first pass and the second pass after reflection off the reflective layer 211 supported by substrate 212. In another embodiment, a similar sheet can be formed as in Fig. 17B by using the structure of the sheet itself formed to the half focal length and coated with reflective coating 213. Other embodiments can include a light-retarding layer 214, as in Fig. 18, so as to rotate or change the polarization state of the light illuminating the sheet upon reflection within the sheet, such as by use of a ¼-wave thin film retarder or waveplate. Further, the reflective optical sheet can be a curved reflective light homogenizing sheet 220 as in Fig. 19. Page 24, lines 7-10, please replace the paragraph with the following amended paragraph:

A method of molding a reflective light homogenizing sheet 210 is illustrated in Fig. 21 such that a transparent polymer sheet 215 and a reflective polymer sheet 216 are embossed and laminated by heat and force applied by two rollers, a cylindrical roller mold 217 and a cylinder mold 218 having a concave microlens surface, then cooled and drawn to form the reflective light homogenizing sheet 210. Another method of fabricating a reflective light homogenizing sheet, as shown in Fig.22A, includes placing UV-curable epoxy 82 between a transparent master mold 50 and a substrate 212 coated with reflective coating 211. By exposing UV light, as shown in Fig. 22B, the reflective sheet 210, shown in Fig. 22C, is formed after being released from the mold. Alternatively, as illustrated in Fig. 23A-23C, a reflective light homogenizing sheet 210 can be molded by the following steps: (1) attaching mold 80(50) and flat mold 92 onto a mold

1	Appl. No. 10/748,618 Amdt. dated Dec. 5, 2005 Reply to Office action of S die, having the ab
2	mold stops are se
3	sheet 210; (2) ap
4	83 or sheet 85 bet
5	as in Fig. 23B; (5
6	applying a reflect
7	molding processe
8	processes as know
9	Page 24 and 25, 1
10	paragraph:
11	Fig. 3 illu
12	adding a subsequ
13	and a second con-
14	108 109 can form
15	within the illumir
16	The first optical s
17	area 112 while the
18	plane 111. Since
19	formed by a proje
20	uniformity can be
21	optical sheets 10

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y to Office action of Sept. 7, 2005 having the ability to adjust stop distance between the molds upon molding, such that the ld stops are set so as to obtain substantially even thickness across the final molded optical et 210; (2) applying mold release 81 to the mold 80(50) and flat mold 92; (3) placing resin or sheet 85 between the molds as in Fig 23A; (4) pressing the die together with force and heat, in Fig. 23B; (5) releasing pressure; (6) removing the optical sheet formed there between; and plying a reflective coating 213 to the flat side. This molding process is applicable to injection olding processes as well as compression molding, transfer molding, and sheet embossing cesses as known in the art. ge 24 and 25, lines 23-15, please replace the paragraph with the following amended

Fig. 3 illustrates an illumination system 109 that uses illumination system 100. By ling a subsequent optical sheet 10 at the illumination plane of illumination system 100, I a second condensing optical system 110 having focal length  $f_{02}$ , the illumination system 3 109 can form uniform intensity output versus position across the illumination plane 111 hin the illuminated area 112 as well as versus angle  $\alpha_1$  within the illuminated area 112. e first optical sheet at plane x<sub>1</sub> creates a top-hat envelope versus angle within illumination a 112 while the second optical sheet forms a uniform top-hat profile at the illumination ne 111. Since the top-hat envelope profile versus angle within illumination plane 112 is med by a projected image of the illuminated tilings across the second optical sheet and formity can be described by how well the input matches the acceptance angle of the sheet, ical sheets 10 having larger pitch tilings can allow more significant intensity fluctuations within the angular envelope. To limit or eliminate this effect, the source output profile versus angle can be forced to be a top-hat as by aperturing or other means, or alternatively, a third

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1	optical sheet 10 can be added either immediately after the source grid array or the source grid
2	array can be imaged with additional optics into this additional optical sheet plane which
3	would be placed at the plane 104.
4	Page 31, lines 15-20, please replace the paragraph with the following amended paragraph:
5	A reflective light homogenizing sheet can be used in a reflective illumination system
6	as shown in Fig. 20, such that input polarized light 232 is imaged through a 3-focal length
7	system having lenses 231 by first with light path being: reflected by a polarizing beamsplitter
8	230; polarization-shifted rotated and reflected by a first reflective light homogenizer;
9	subsequently polarization-shifted rotated and reflected by a subsequent reflective light
10	homogenizer; and then reflected by the polarization beamsplitter into a uniform output plane
11	233 both uniform versus position as well as versus angle.
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